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# Carbon dioxide capture and conversion by an acid-base resistant metal-organic framework

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Considering the rapid increase of CO<sub>2</sub> emission, especially from power plants, there is a constant need for materials which can effectively eliminate post-combustion CO<sub>2</sub> (the main component: CO<sub>2</sub>/N<sub>2</sub> = 15/85). Here, we show the design and synthesis of a Cu(II) metal-organic framework (**FJI-H14**) with a high density of active sites, which displays unusual acid and base stability and high volumetric uptake (171 cm<sup>3</sup> cm<sup>-3</sup>) of CO<sub>2</sub> under ambient conditions (298 K, 1 atm), making it a potential adsorbing agent for post-combustion CO<sub>2</sub>. Moreover, CO<sub>2</sub> from simulated post-combustion flue gas can be smoothly converted into corresponding cyclic carbonates by the **FJI-H14** catalyst. Such high CO<sub>2</sub> adsorption capacity and moderate catalytic activity may result from the synergistic effect of multiple active sites.

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Due to the dependence on fossil fuels to meet the world's growing energy demand, the concentration of CO<sub>2</sub> in the atmosphere has increased from 310 p.p.m. to over 380 p.p.m. during the last half century, and it continues to rise<sup>1–3</sup>. Some 60% of the total CO<sub>2</sub> emission worldwide is attributable to electricity generation<sup>4</sup>. The installation of effective CO<sub>2</sub> capture systems that can selectively remove the CO<sub>2</sub> component of the exhaust gas emitted by coal- or gas-fired power plants would extremely reduce the global annual emissions. Current technologies involving aqueous amine absorbents for the capture of CO<sub>2</sub> from a gas mixture are usually themselves significant consumers of energy and a source of corrosion problems in equipment<sup>5–7</sup>. Thus, exploration of new materials that can selectively and efficiently eliminate combustion-generated CO<sub>2</sub> is urgent.

Due to their large capacity for the adsorption of gases and their chemical tunability<sup>8–21</sup>, the emerging porous metal-organic frameworks (MOFs) could serve as promising cost-effective and efficient materials for CO<sub>2</sub> capture and separation, but development of practically useful MOF materials for CO<sub>2</sub> capture directly from power plants remains a challenge. The flue gas generated from coal-fired power plant, released at a total pressure of approximately 1 atm., contains 15–16% CO<sub>2</sub>, 73–77% N<sub>2</sub>, 5–7% H<sub>2</sub>O, 3–4% O<sub>2</sub> and a small amount of acid gas<sup>22–24</sup>. An ideal MOF material for CO<sub>2</sub> capture should exhibit extraordinarily high CO<sub>2</sub> uptake and selectivity at ambient pressures; furthermore, it should also be resistant to water and acid gas, can be prepared on a large scale and is reusable. Moreover, in terms of practical applications, high volumetric CO<sub>2</sub> adsorption capacity seems even more important than gravimetric CO<sub>2</sub> adsorption capacity, since the capture and separation of post-combustion CO<sub>2</sub> is often carried out in a fixed-bed reactor<sup>5</sup>.

Generally, open metal sites (OMS) and Lewis basic sites (LBS) are favorable for interaction with CO<sub>2</sub> and various types of OMS and LBS have been introduced into MOFs in an effort to improve their adsorption capacity<sup>25–32</sup>. To adsorb CO<sub>2</sub> effectively under ambient conditions, one would seek to prepare an MOF with high densities of OMS and LBS, in which the OMS and LBS could synergistically capture CO<sub>2</sub> molecules in the pores. Such a potential synergy effect from the OMS and LBS can improve the adsorption capacity more effectively than a single OMS or LBS.

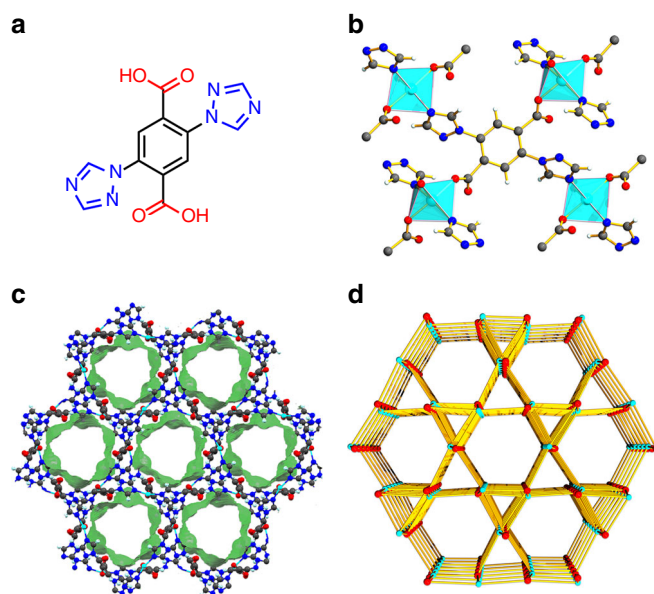
In this paper, we describe the design and synthesis of a Cu(II)-MOF, **FJI-H14** with a high density of OMS and LBS, which shows extraordinary high volumetric uptake of CO<sub>2</sub> at ambient conditions and excellent selectivity for CO<sub>2</sub> over N<sub>2</sub>. Remarkably, it is highly stable in a water and acid/base environment and can be reused without loss of adsorption capacity; furthermore, it can be easily synthesized in large quantities. Experiments with simulated post-combustion flue gas have shown that **FJI-H14** can smoothly catalyze the chemical transformation of CO<sub>2</sub> into the corresponding cyclic carbonates.

## Results

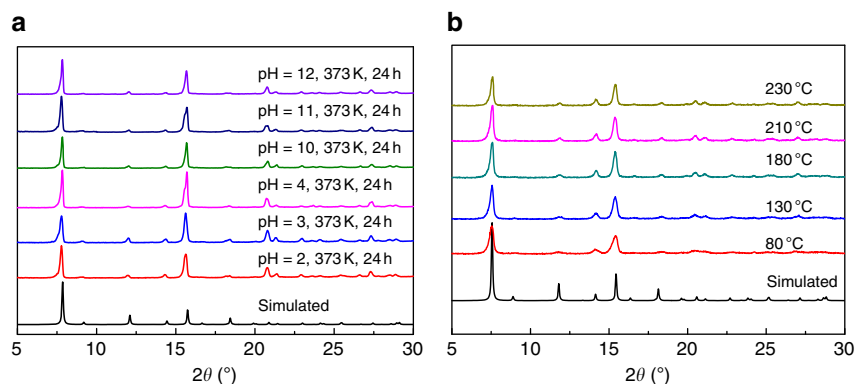
**Synthesis and structure analysis.** The reaction of 2,5-di(1*H*-1,2,4-triazol-1-yl)terephthalic acid (H<sub>2</sub>BTTA, Fig. 1a) with Cu(NO<sub>3</sub>)<sub>2</sub> in H<sub>2</sub>O at 120 °C for 3 days affords rod-shaped blue crystals of **FJI-H14** ([Cu(BTTA)H<sub>2</sub>O]<sub>n</sub>·6nH<sub>2</sub>O) in 73% yield. Single-crystal X-ray structure analysis shows that **FJI-H14** crystallizes in trigonal space group *R*-3 (for more details see Supplementary Table 1). The crystallographic asymmetric unit contains one BTTA<sup>2-</sup> ligand, one Cu(II) ion and one coordinate water. As shown in Fig. 1b, each Cu(II) ion has a square-pyramidal coordination geometry, and is surrounded by two imine N atoms from two different 1,2,4-triazole groups and two O atoms from two different carboxylate groups in the equatorial plane, together with one O atom of the water molecule in the

vertex (Supplementary Fig. 1). Topologically, the Cu(II) ion is a planar 4-connected node, further linked by four tetradentate BTTA<sup>2-</sup> ligands into a three-dimensional network with Kagome-like **USF** topology (Fig. 1d). Consequently, there are hexagonal one-dimensional channels along the *c* direction (Fig. 1c). The pore limiting diameter and the maximum pore diameter predicted by the program Poreblazer<sup>33</sup> for the fully evacuated **FJI-H14** are 5.95 and 7.62 Å, respectively. The evacuated **FJI-H14** has a theoretical porosity of 44.4% according to PLATON calculations with a probe radius of 1.65 Å. **FJI-H14** has a total concentration of active sites as high as 9.22 mol l<sup>-1</sup> (the total of Cu(II) OMS is 3.07 mol l<sup>-1</sup> and free N LBS is 6.15 mol l<sup>-1</sup>), which is higher than in many well-known MOFs for CO<sub>2</sub> capture (Supplementary Table 2).

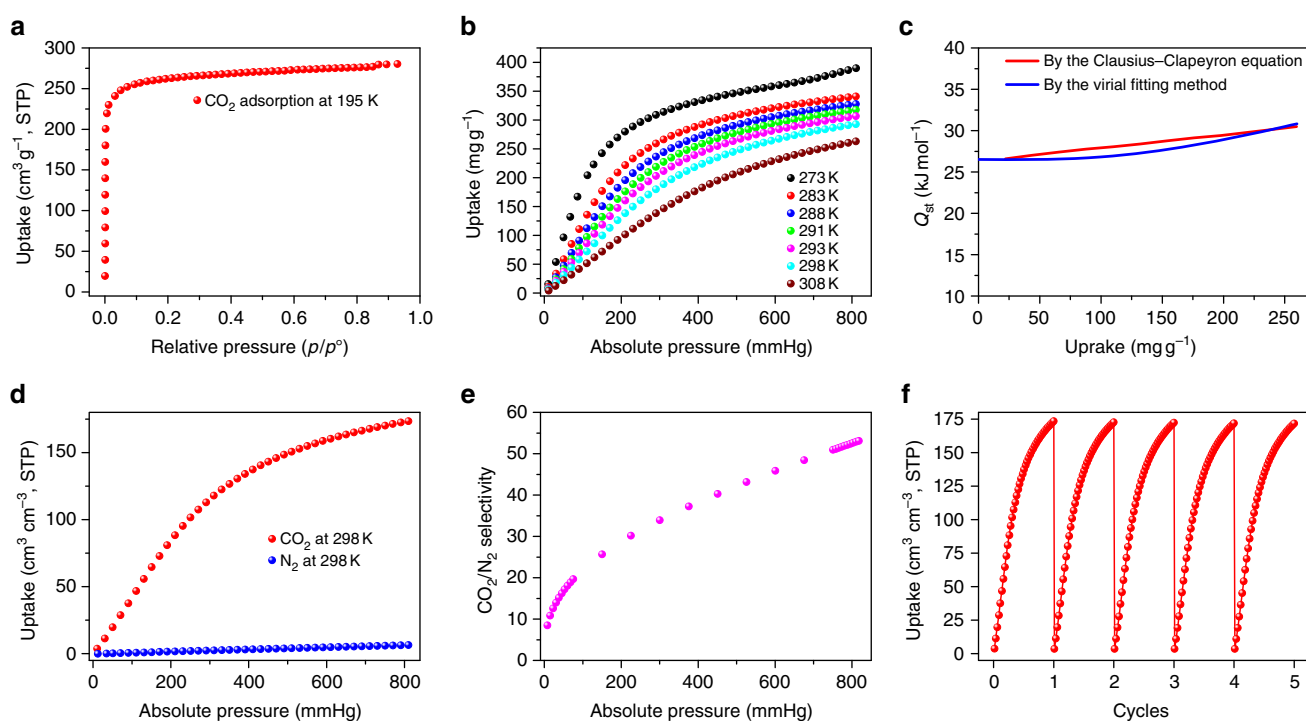
**Stability.** The flue gas from power plants contains moisture and acid gas, suggesting that the practical adsorbents of post-combustion CO<sub>2</sub> should be sufficiently stable toward heat, water and acid. This led us to investigate both the chemical stability and thermal stability of **FJI-H14** before the CO<sub>2</sub> adsorption test. Powder X-ray diffraction pattern (PXRD) analyses reveal that **FJI-H14** is very stable not only in boiling water but also in both acid and base environments at pH = 2 to pH = 12 and at temperatures as high as 373 K (Fig. 2a). However, the framework of **FJI-H14** collapses when it is immersed for 24 h in solution at pH = 1 or pH = 13 (Supplementary Fig. 2). Thermogravimetric analysis (TGA) studies (Supplementary Fig. 3) indicate that the as-synthesized **FJI-H14** sample is thermally stable up to 230 °C, and this is confirmed by temperature-dependent PXRD studies (Fig. 2b and Supplementary Fig. 4). Generally, MOFs based on Cu ions and organic carboxylates are usually subject to hydrolysis in the presence of moisture and only a few known MOFs show such excellent chemical stability<sup>16, 34–38</sup>. The unusual chemical stability of **FJI-H14** may result from its unique structure because the penta-coordinated Cu(II) ion subunit should be more stable than



**Fig. 1** Structural illustration of **FJI-H14**. **a** The selected ligand H<sub>2</sub>BTTA for the construction of **FJI-H14**. **b** The coordination environment of the Cu(II) ions as four-connected nodes and BTTA also as a four-connected node. **c** The one-dimensional nanoporous channels along the crystallographic *c* direction. **d** The framework of **USF** topology. (Cu atom, cyan; C atom, gray; O atom, red; N atom, blue; H atom, white)



**Fig. 2** Stability of FJI-H14. **a** PXRD patterns after treatment with boiling water, acid/base environment from pH = 2 to 12 at 373 K. **b** Temperature-dependent PXRD patterns



**Fig. 3** Experimental  $\text{CO}_2$  adsorption by FJI-H14. **a**  $\text{CO}_2$  adsorption isotherm for FJI-H14 at 195 K. **b**  $\text{CO}_2$  adsorption isotherm for FJI-H14 at 273, 283, 288, 291, 293, 298 and 308 K. **c** The isosteric heat of  $\text{CO}_2$  adsorption ( $Q_{st}$ ) for FJI-H14 calculated by the Clausius-Clapeyron equation and the Virial fitting method. **d**  $\text{N}_2$  and  $\text{CO}_2$  adsorption isotherms for FJI-H14 at 298 K. **e**  $\text{CO}_2/\text{N}_2$  selectivity for the 15/85  $\text{CO}_2/\text{N}_2$  mixture at 298 K. **f** Cycles of  $\text{CO}_2$  adsorption for FJI-H14 at 298 K

traditional paddle-wheel structure due to the Cu–N coordination interaction, which is stronger than the Cu–O interaction. Furthermore, the abundant free N atoms could also prevent the destruction caused by acids.

**Porosity and  $\text{CO}_2$  adsorption capacity.** The FJI-H14 sample for adsorption testing was pre-activated under dynamic vacuum at 100 °C for 10 h after exchanged by acetone for 3 days. PXRD data displayed that the crystallinity was retained after activation (Supplementary Fig. 5).  $\text{N}_2$  adsorption at 77 K was much lower than expected (Supplementary Fig. 6), and consequently, the porosity of activated FJI-H14 was examined by  $\text{CO}_2$  adsorption experiments at 195 K. A  $\text{CO}_2$  uptake of 279  $\text{cm}^3 \text{g}^{-1}$  was obtained (Fig. 3a), corresponding to a formula  $[\text{Cu}(\text{BTAA})_n \cdot 4.5n\text{CO}_2$ . A

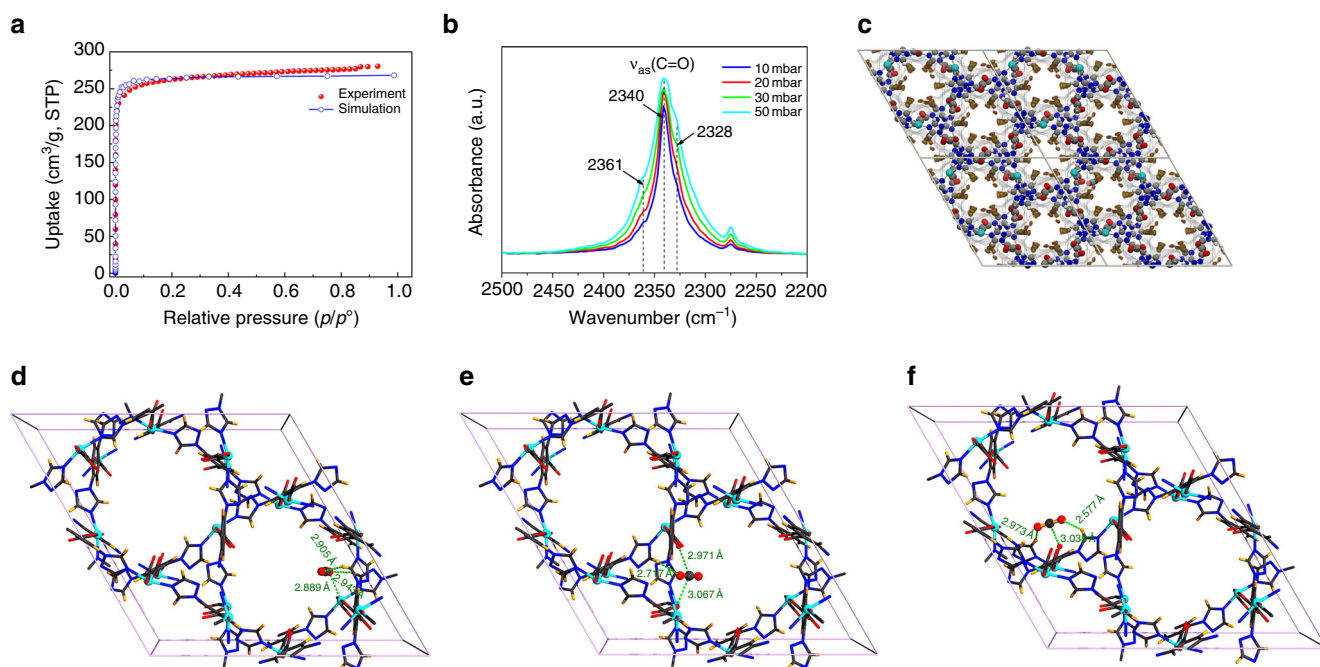
phenomenon that restricted  $\text{N}_2$  uptake at 77 K but supported type-I  $\text{CO}_2$  uptake at 195 K has been observed in several reported MOF materials (Supplementary Table 3). However, FJI-H14 has a low  $\text{N}_2$  uptake of 170  $\text{cm}^3 \text{g}^{-1}$  at 77 K and 1 atm, which is different from the reported MOFs which exhibit almost zero  $\text{N}_2$  adsorption at 77 K. The much lower  $\text{N}_2$  adsorption at 77 K of FJI-H14 may be a consequence of the relatively narrow pores in FJI-H14 being easily blocked by the relatively large  $\text{N}_2$  molecule at 77 K, so hindering further diffusion of  $\text{N}_2$  into the framework of FJI-H14. The typical type-I isotherm observed indicates that only micropores are formed in the framework of activated FJI-H14. The Brunauer–Emmett–Teller (BET)-specific surface area of FJI-H14 is calculated to be 904  $\text{m}^2 \text{g}^{-1}$  and its Langmuir-specific surface area is 1004  $\text{m}^2 \text{g}^{-1}$ . The total pore volume estimated from the experimental  $\text{CO}_2$  isotherm is 0.45  $\text{cm}^3 \text{g}^{-1}$  at  $P/P_0 = 0.92$ ,

which is slightly higher than the theoretical value of  $0.39 \text{ cm}^3 \text{ g}^{-1}$  derived from the solvent accessible volume and the crystal density through PLATON calculations with a probe radius of  $1.65 \text{ \AA}$ . The comparable values of the pore volume indicate that the activated **FJI-H14** remains permanently porous.

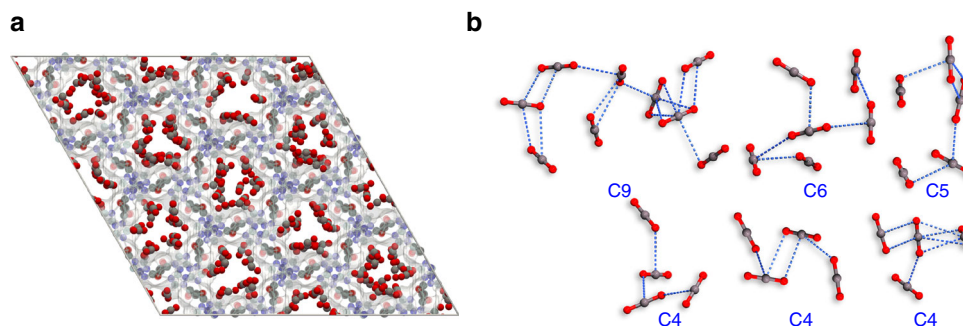
The incorporation of high porosity and the high concentration of open active sites in the framework are expected to lead to high  $\text{CO}_2$  uptake. Indeed, activated **FJI-H14** exhibits remarkable  $\text{CO}_2$  volumetric adsorption capacities of  $171 \text{ cm}^3 \text{ cm}^{-3}$  at  $298 \text{ K}$  and  $1 \text{ atm}$  (Fig. 3d), and the capacity is only lower than that of **MAF-X25ox** ( $203 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>36</sup>, **MAF-X27ox** ( $196 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>36</sup> and **Co<sub>2</sub>(dobdc)** ( $184 \text{ cm}^3 \text{ cm}^{-3}$ ) under the same conditions<sup>36, 39</sup>, exceeding that in almost all well-known MOFs such as **Mg-MOF-74** ( $162 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>6, 40</sup>, **UTSA-16** ( $160 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>6, 41</sup>, **SIFSIX-2-Cu-i** ( $151 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>42</sup>, **MPM-1-TIFSIX** ( $115.7 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>43</sup>, **Bio-MOF-11** ( $113 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>6, 44</sup>, **Cu-tdpat** ( $103 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>6, 45</sup> and **Mmen-CuBTTri** ( $83 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>6, 30</sup> (Supplementary Table 2). The formula of  $\text{CO}_2$  adsorbed **FJI-H14** at room temperature is  $[\text{Cu}(\text{BTTA})]_n \cdot 2.4n\text{CO}_2$  and there is a 53%  $\text{CO}_2$  occupancy at room temperature compared with the maximal uptake at  $195 \text{ K}$ , which is rather high compared with reported MOFs such as **SMT-1** (27%)<sup>46</sup>,  $[\text{Cu}(\text{L})]$  (31%)<sup>47</sup> and **MPM-1-Cl** (29%)<sup>43</sup>. It should be noted that although volumetric adsorption capacity is more practical for stationary  $\text{CO}_2$  capture and separation applications, the gravimetric adsorption capacity is also an important parameter for  $\text{CO}_2$  capture. Although the gravimetric  $\text{CO}_2$  uptake of **FJI-H14** ( $146 \text{ cm}^3 \text{ g}^{-1}$ ) is lower than that of **Mg-MOF-74** ( $176 \text{ cm}^3 \text{ g}^{-1}$ ) due to the considerably lighter weight of **Mg**<sup>40</sup>, it can be comparable to that in other familiar MOF materials such as **MAF-X25ox** ( $160 \text{ cm}^3 \text{ g}^{-1}$ )<sup>36</sup>,  $[\text{Co}_2(\text{dobdc})]$  ( $154 \text{ cm}^3 \text{ g}^{-1}$ )<sup>39</sup> or **MAF-X27ox** ( $150 \text{ cm}^3 \text{ g}^{-1}$ )<sup>36</sup>. Another challenging issue is the uptake of  $\text{CO}_2$  at low pressure, which can be highly improved by chemisorption due to the stronger interactions. For instance, the hydrazine functionalized MOF  $[\text{Mg}_2(\text{dobdc})(\text{N}_2\text{H}_4)_{1.8}]$  ( $137 \text{ cm}^3 \text{ cm}^{-3}$ ) developed by Zhang et al. shows the highest volumetric  $\text{CO}_2$  adsorption capacities at

$298 \text{ K}$  and  $0.15 \text{ bar}$ <sup>31</sup>, and the second highest is **MAF-X27ox** ( $124 \text{ cm}^3 \text{ cm}^{-3}$ )<sup>36</sup>, which was also prepared by Zhang et al. Based on physisorption, **FJI-H14** displays a volumetric capacity of  $60 \text{ cm}^3 \text{ cm}^{-3}$  at  $298 \text{ K}$  and  $0.15 \text{ atm}$ , which makes it comparable to **SIFSIX-2-Cu-i** ( $63 \text{ cm}^3 \text{ cm}^{-3}$ ). In order to evaluate the affinity of the pore surface of activated **FJI-H14** toward  $\text{CO}_2$ , the isosteric heat of adsorption ( $Q_{\text{st}}$ ) of activated **FJI-H14** was calculated using the Clausius–Clapeyron equation based on the  $\text{CO}_2$  isotherms at seven different temperatures without data fitting (Fig. 3b, Supplementary Fig. 7 and Supplementary Table 4). As shown in Fig. 3c, the  $Q_{\text{st}}$  at low coverage is  $26.6 \text{ kJ mol}^{-1}$  and then slightly increases to  $30.5 \text{ kJ mol}^{-1}$  with  $\text{CO}_2$  loading increasing to  $260 \text{ mg g}^{-1}$ . The  $Q_{\text{st}}$  with an increasing slope is unusual<sup>9, 36, 43, 48</sup>, and reveals the possible formation of  $\text{CO}_2$  clusters inside the pores. Such phenomena have been previously observed in other porous MOFs materials<sup>41, 49</sup>. The  $Q_{\text{st}}$ , confirmed by the Virial fitting method<sup>50</sup>, also slowly increases from  $26.5$  to  $30.8 \text{ kJ mol}^{-1}$  with increasing  $\text{CO}_2$  loading from lower coverage to  $260 \text{ mg g}^{-1}$  (Fig. 3c and Supplementary Fig. 8). Such similar trends in the two methods confirm the unusual increasing slope in  $Q_{\text{st}}$ .

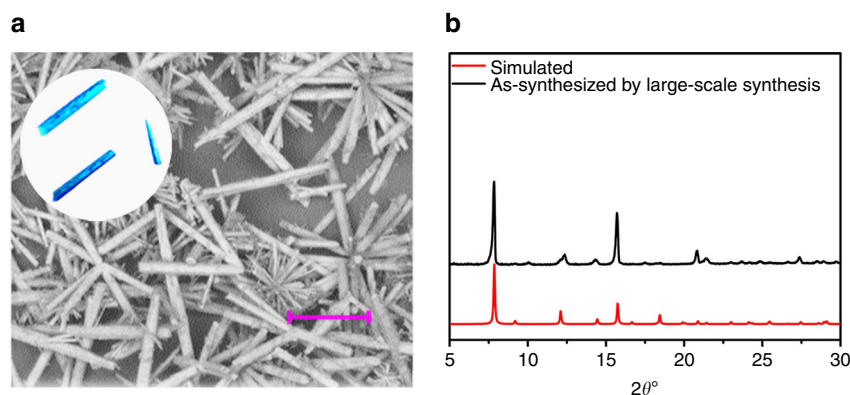
Because flue gas from power plants contains a large amount of  $\text{N}_2$ , the  $\text{CO}_2/\text{N}_2$  selectivity is a crucial parameter in  $\text{CO}_2$  capture applications. For comparison,  $\text{N}_2$  sorption isotherms were also measured at  $298 \text{ K}$ , and showed an uptake of  $6.5 \text{ cm}^3 \text{ cm}^{-3}$  at  $1 \text{ atm}$  (Fig. 3d). By the ideal adsorbed solution theory (IAST)<sup>51</sup>, the  $\text{CO}_2/\text{N}_2$  selectivity for the 15/85  $\text{CO}_2/\text{N}_2$  mixture at  $1 \text{ atm}$  is calculated to be 51 at  $298 \text{ K}$  (Fig. 3e). The highly selective adsorption of  $\text{CO}_2$  over  $\text{N}_2$  further suggests that the densely populated open active sites in the framework have a positive effect on  $\text{CO}_2$  adsorption. The possibility of reuse of an adsorbent is also an important aspect of the practical application. Further research demonstrates that activated **FJI-H14** can be recycled without losing its adsorption capacity. Even after five cycles, it still maintains 100% adsorption capacity as shown in Fig. 3f, indicating that **FJI-H14** is highly suitable for  $\text{CO}_2$  capture.



**Fig. 4** Mechanism of  $\text{CO}_2$  adsorption of **FJI-H14**. **a** Experimental and simulated excess  $\text{CO}_2$  adsorption isotherms at  $195 \text{ K}$ . **b** Background-subtracted FTIR spectra of  $\text{CO}_2$  adsorbed on **FJI-H14** at decreasing equilibrium pressure. **c** Density picture of adsorbed  $\text{CO}_2$  ( $1 \text{ CO}_2$  at  $273 \text{ K}$ ), which is shown as a volume rendered mode. **d–f** represent three preferential  $\text{CO}_2$  locations in **FJI-H14** obtained from GCMC simulation and DFT optimization



**Fig. 5** The snapshot for CO<sub>2</sub>-loaded FJI-H14. **a** The snapshot of CO<sub>2</sub> adsorption for **FJI-H14** at 11.2 kPa and 273.15 K calculated using the GCMC method. **b** The representative CO<sub>2</sub> clusters including nine (C9), six (C6), five (C5) and four (C4) CO<sub>2</sub> molecules. The blue dashed line represents weak interactions between neighboring CO<sub>2</sub> molecules with a short C...O separation (from 2.71 to 3.50 Å) for adjacent CO<sub>2</sub> molecules



**Fig. 6** Large-scale synthesis of FJI-H14 microcrystals. **a** Morphology comparison between SEM image of **FJI-H14** microcrystals and of **FJI-H14** single crystals (inset). Scale bars, 10 μm. **b** PXRD patterns comparison: black represents simulated **FJI-H14**; red represents **FJI-H14** microcrystals

**Revealing the CO<sub>2</sub> adsorption sites in FJI-H14.** The extraordinary CO<sub>2</sub> capture performance of **FJI-H14** under ambient conditions has motivated us to rationalize the crucial factors supporting the high CO<sub>2</sub> adsorption capacity. To understand the sorption behavior of **FJI-H14**, both grand canonical Monte Carlo (GCMC) simulations and density functional theory (DFT) calculations have been carried out and are shown in Fig. 4. The GCMC simulations show that the theoretical CO<sub>2</sub> adsorption isotherms of **FJI-H14** are basically consistent with the experimental data at different temperatures (195, 273 and 298 K) (Fig. 4a, Supplementary Fig. 9). The simulated CO<sub>2</sub> concentration loaded into **FJI-H14** is about 4.3, 3.1 and 2.5 CO<sub>2</sub> per ligand molecule at 195, 273 and 298 K, respectively. These figures are close to the experimental values of 4.5, 3.1 and 2.4 CO<sub>2</sub> per ligand molecule at 195, 273 and 298 K. As shown in Fig. 4c, the adsorbed CO<sub>2</sub> molecules at low coverage prefer to locate the corners of hexagonal channels. Combining the density plots and a snapshot of the adsorbed CO<sub>2</sub> molecules, three typical preferential CO<sub>2</sub> adsorption sites can be observed. These three adsorption sites were further optimized by DFT methods using the Dmol<sup>3</sup> module. Site I (Fig. 4d) shows that CO<sub>2</sub> molecules prefer to coordinate with open Cu(II) ions through Cu–O interaction, with a Cu–O distance of about 2.889 Å, and each copper site binding only one CO<sub>2</sub><sup>52</sup>. In Site II (Fig. 4e), the two closest C–O distances are about 2.971 and 3.067 Å, indicating that O atoms of carboxyl group could also interact as a Lewis base with CO<sub>2</sub>. It is also interesting to find that positively charged H atoms could further promote CO<sub>2</sub> adsorption, with the shortest O–H distances about 2.577 Å as shown in Site III (Fig. 4f). The calculated static CO<sub>2</sub> binding

energy of the above three different preferential CO<sub>2</sub> adsorption sites are ~43.71, 38.94, 32.82 kJ mol<sup>-1</sup>, respectively, indicating that the open copper sites could play a leading role in CO<sub>2</sub> adsorption.

The simulated  $Q_{st}$  from the GCMC simulations can be used to deduce the information on  $Q_{st}$  with an increasing slope for **FJI-H14**. As shown in Supplementary Fig. 10, the simulated  $Q_{st}$  of 30.7–34.6 kJ mol<sup>-1</sup> is slightly larger than suggested by experimental results and has a uniformly increasing trend with increasing CO<sub>2</sub> loading. The contribution of the CO<sub>2</sub>...Framework interaction to the total  $Q_{st}$  decreases slightly with increasing loading, which is reasonable because CO<sub>2</sub> molecules first occupied the more active sites. However, the contribution from the CO<sub>2</sub>...CO<sub>2</sub> interactions shows a tendency to increase significantly from 0 to 7.0 kJ mol<sup>-1</sup>, which is due to the closer packing of the CO<sub>2</sub> molecules under the higher pressure in the relatively narrow pores. Hence, the behavior of the total  $Q_{st}$  is the result of the two cooperative contributions. The increasing contribution from the CO<sub>2</sub>...CO<sub>2</sub> interactions indicates that the CO<sub>2</sub> clusters could have formed inside the pores. Hence, GCMC simulation was used to investigate the potential CO<sub>2</sub> clusters. Some small CO<sub>2</sub> clusters can be found in the snapshot at 195 K and low pressure (~21 Pa) calculated using the GCMC method (Supplementary Fig. 11), but at 273 K, similar CO<sub>2</sub> clusters can only be observed under a relatively high pressure of 11 kPa. The snapshots of the framework of **FJI-H14** with CO<sub>2</sub> molecules adsorbed are shown in Fig. 5a. The weak interactions between neighboring CO<sub>2</sub> molecules are found in terms of the short C...O separation (from 2.71 to 3.50 Å) for adjacent CO<sub>2</sub> molecules,

**Table 1 Cyclic carbonates from epoxides and CO<sub>2</sub><sup>a</sup>**

Entry	Substrates	Catalysts	t[h]	Yield(%) <sup>b</sup>
1		<b>FJI-H14</b>	24	86
2		–	24	52
3		Cu(OAc) <sub>2</sub>	24	45 <sup>c</sup>
4		Cu(NO <sub>3</sub> ) <sub>2</sub> <sup>+</sup> H <sub>2</sub> BTTA	24	70
5		HKUST-1	24	67
6		<b>FJI-H14</b>	24	95
7		<b>FJI-H14</b>	24	27

<sup>a</sup>Reaction conditions: styrene oxide (20.0 mmol), catalyst (0.48 mol% per Cu(II) units), TBAB (2.5 mol%) in a Schleck tube with condenser, 1 atm simulated post-combustion flue (CO<sub>2</sub> = 0.15 atm, N<sub>2</sub> = 0.85 atm) was bubbled at 80 °C for 24 h

<sup>b</sup>Determined by <sup>1</sup>H NMR.

<sup>c</sup>Some by-products were found when Cu(OAc)<sub>2</sub> was used as a catalyst

which links those CO<sub>2</sub> molecules into small clusters (Fig. 5b and Supplementary Fig. 12).

To verify the preferential adsorption sites experimentally, in situ fourier transform infrared microscope (FT-IR) spectra of activated **FJI-H14** sample have been collected at increasing equilibrium pressure under a CO<sub>2</sub> atmosphere. Figure 4b shows the background-subtracted IR spectra obtained by the progressive lowering of equilibrium pressure at room temperature. The strong absorption bands at 2,340 and 2,328 cm<sup>-1</sup> red-shifted by Δν of about -9 and -21 cm<sup>-1</sup> from gas phase CO<sub>2</sub> asymmetric stretch (ν<sub>as</sub> = 2349 cm<sup>-1</sup>) might be attributed to the ν<sub>as</sub> mode of

CO<sub>2</sub> (Supplementary Fig. 13) interacting with Cu(II) centers. The slightly blue-shifted band at 2,361 cm<sup>-1</sup> (Δν = +12 cm<sup>-1</sup> shift) can be readily assigned to the asymmetric ν<sub>as</sub> stretch of CO<sub>2</sub> interacting with the exposed Lewis base sites throughout the channel. On the low-frequency side of this main absorption, the less intense bands at 2,275 cm<sup>-1</sup> result from the interaction between Cu(II) center and <sup>13</sup>CO<sub>2</sub> which is present (1%) naturally in <sup>12</sup>CO<sub>2</sub>. The stronger absorption bands at 2,340 cm<sup>-1</sup> and 2,328 cm<sup>-1</sup> also indicate that CO<sub>2</sub> molecules tend to stack around the open Cu(II) sites, which is in accord with the above theoretical calculation.

**Large-scale synthesis.** For practical applications, efficient macroscopic preparation and purification are a bottleneck problem which must be solved. After many attempts, the following protocol for large-scale preparation of **FJI-H14** has been established: by directly mixing  $\text{H}_2\text{BTTA}$  ligand and  $\text{Cu}(\text{NO}_3)_2$  in water and then refluxing for 1 day, microcrystalline **FJI-H14** can be obtained with a high yield of 90%, its purity confirmed by PXRD analysis (Fig. 6b). Scanning electron microscopy measurements demonstrate that the relatively uniform rod crystallites form on the scale of about 20  $\mu\text{m}$ , displaying a similar morphology with the single crystal (Fig. 6a) obtained from the hydrothermal reaction. Therefore, macroscopic samples of **FJI-H14** even on a 10 g scale can be readily synthesized by this method, which makes its application more possible.

### Catalyzed cycloaddition of $\text{CO}_2$ using flue gas as feedstock.

Another attractive means of effective elimination of  $\text{CO}_2$  is the direct chemical conversion of  $\text{CO}_2$  into value-added chemicals, such as dimethyl carbonate, cyclic carbonates,  $N,N'$ -disubstituted ureas or formic acid. Given their wide applications in the pharmaceutical and fine chemical industries, cyclic carbonates formed by the coupling of epoxides with  $\text{CO}_2$  have attracted intense interest. Although several existing MOFs have been shown to be excellent heterogeneous Lewis acid catalysts for chemical conversion of  $\text{CO}_2$  either at high pressure or normal pressure<sup>53–56</sup>, the exploration of practically useful MOF materials which can catalyze the conversion of  $\text{CO}_2$  obtained directly from power plants remains a challenge to be addressed. The high density of OMSs and LBSs which are finely distributed throughout the channel pores of **FJI-H14**, are devoted to capturing  $\text{CO}_2$  effectively and selectively under ambient conditions. Such unusual synergistic effects may also improve chemical conversion of post-combustion  $\text{CO}_2$  from the power plant. Here, we use a mixed gas which contains 0.15 atm  $\text{CO}_2$  and 0.85 atm  $\text{N}_2$  to simulate flue gas from the power plant. As expected, **FJI-H14** displays a much higher catalytic activity for cycloaddition of styrene oxide with the simulated flue gas than other catalysts, such as homogeneous  $\text{Cu}(\text{OAc})_2$ , heterogeneous HKUST-1 and a mixture of  $\text{Cu}(\text{NO}_3)_2$  and free  $\text{H}_2\text{BTTA}$  ligand. As shown in Table 1, absence of extra Lewis acid catalysts only lead to a moderate yield (52%), while use of extra  $\text{Cu}(\text{II})$  catalyst can improve their reaction activity, with the exception of  $\text{Cu}(\text{OAc})_2$ . Catalyzed by **FJI-H14**, chemical conversion of diluted  $\text{CO}_2$  with styrene oxide into corresponding cyclic carbonates gives a yield of 86% within 24 h, while use of homogeneous  $\text{Cu}(\text{OAc})_2$  and the mixture of  $\text{Cu}(\text{NO}_3)_2$  and  $\text{H}_2\text{BTTA}$  leads only to 45 and 70% yields respectively under the same reaction conditions. Further tests demonstrate that the **FJI-H14** is more active than well-known HKUST-1 which leads to only 67% yield under the same conditions. All these results indicate that **FJI-H14** is indeed an efficient catalyst for chemical conversion of  $\text{CO}_2$  under practical conditions. In order to investigate the catalytic character of **FJI-H14**, another two different sized substrates have been selected. As shown in Table 1 entries 5–6, the smaller (chloromethyl)ethylene oxide gives a higher yield (95%), while 1,2-epoxyoctane leads to a lower yield (27%), indicating that the cycloaddition reaction may occur within the pores of **FJI-H14**, into which smaller-sized substrates could easily diffuse and make contact with the active sites. To further prove that the reaction may occur in the pores of **FJI-H14**, uptake of different reactants has also been assessed. Further analysis demonstrates that (chloromethyl)ethylene oxide indeed diffuses into the pores of **FJI-H14** more easily than 1,2-epoxyoctane and styrene oxide which apparently have similar diffusion rates. Considering the similar diffusion from 1,2-epoxyoctane and styrene oxide, the higher activity of styrene

oxide compared to 1,2-epoxyoctane may result from following two factors: first, a phenyl ring is an electron-withdrawing group, which can improve reaction activity, and second, the  $\pi$ - $\pi$  interaction from the phenyl ring of styrene oxide and the aromatic rings of the **FJI-H14** framework also can improve reaction activity. This may provide a strategy for development of more practical catalysts for the conversion of  $\text{CO}_2$  directly from flue gas.

### Discussion

Considering that most of  $\text{CO}_2$  emission is generated from power stations, direct elimination of such  $\text{CO}_2$  should play an important role in the reduction of global  $\text{CO}_2$  emissions. The characteristics and composition of post-combustion  $\text{CO}_2$  determine that an ideal adsorbent for post-combustion  $\text{CO}_2$  capture should possess advantages such as high  $\text{CO}_2$  uptake and selectivity at ambient pressure, excellent chemical stability and thermal stability, good reusability and large-scale production with low cost. Porous MOFs have been proved to be effective adsorbents for  $\text{CO}_2$  capture due to their large capacity for the adsorption of gases, but development of an ideal MOF for post-combustion  $\text{CO}_2$  capture is still challenging. Although many different OMS and LBS have been introduced into MOFs to improve  $\text{CO}_2$  capture, only very few porous MOFs have been realized for high  $\text{CO}_2$  capture at ambient conditions, and most of them are sensitive to water. **FJI-H14** not only shows extraordinary high volumetric uptake of  $\text{CO}_2$  with high selectivity under ambient conditions but is also highly resistant to water and an acid/base environment; furthermore, it also can be reused without loss of adsorption capacity and prepared on a large-scale with low cost. These advantages make **FJI-H14** an ideal and practical adsorbent for post-combustion  $\text{CO}_2$ . An unusual synergistic effect from multiple active sites has also been observed, and may provide a strategy for the design of more effective adsorbents for  $\text{CO}_2$  capture. Further chemical conversion of captured  $\text{CO}_2$  to high-value products, such as cyclic carbonate, is also attractive, and several existing MOFs have been proved to be excellent heterogeneous Lewis acid catalysts for chemical conversion of pure  $\text{CO}_2$ . However, development of MOF materials which can catalyze the direct conversion of post-combustion  $\text{CO}_2$  still remains a challenge. It is shown here that **FJI-H14** can directly and smoothly catalyze the chemical transformation of simulated post-combustion gas  $\text{CO}_2$  into corresponding cyclic carbonates. All these results should be instructive for the design and discovery of more effective and practical MOF materials for the elimination of post-combustion  $\text{CO}_2$  in the near future.

### Methods

**Synthesis and scale up.** A mixture of  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$  (0.05 mmol, 12 mg) and  $\text{H}_2\text{BTTA}$  (0.05 mmol, 15 mg) in  $\text{H}_2\text{O}$  (4 ml) was sealed in a 23 mL Teflon vial, which was heated at 120 °C for 3 days, then cooled to room temperature. After washing with fresh acetone, blue crystals of **FJI-H14** were obtained in 73% yield based on the organic ligand  $\text{H}_2\text{BTTA}$ . Elemental analysis was calculated for **FJI-H14**: C, 29.54%; H, 4.13%; N, 17.23%. Found: C, 29.35%; H, 4.12%; N, 17.29%. For scale up, a mixture of  $\text{Cu}(\text{NO}_3)_2 \cdot 3\text{H}_2\text{O}$  (1 mmol, 241.6 mg) and  $\text{H}_2\text{BTTA}$  (1 mmol, 300.1 mg) in  $\text{H}_2\text{O}$  (80 ml) was refluxed for 1 day, and then the blue powder of **FJI-H14** microcrystals could be obtained in 90% yield based on  $\text{H}_2\text{BTTA}$ . After three washings with water and two with acetone, the phase purity of the sample was confirmed by PXRD.

**Characterization.** Elemental analyses for C, H, N were carried out on a German Elementary Vario EL III instrument. The  $^1\text{H}$  NMR spectra were measured on an AVANCE III Bruker Biospin spectrometer, operating at 400 MHz. Thermogravimetric analyses (TGA) were recorded on an NETZSCH STA 449 C unit at a heating rate of 10 °C  $\text{min}^{-1}$  under flowing nitrogen atmosphere. In situ FT-IR spectra were obtained using a NICOLET 6700 instrument at 298 K. The PXRD patterns were collected using a Rigaku MiniFlex 600 X-ray diffractometer with monochromatic  $\text{Cu K}\alpha$  radiation ( $\lambda = 1.54 \text{ \AA}$ ). Simulations of the PXRD spectrum were carried out by the single-crystal data and diffraction-crystal module of the

Mercury program, available free of charge via the internet at <https://www.ccdc.cam.ac.uk/solutions/csd-system/components/mercury/>.

**Single-crystal X-ray diffraction.** The single-crystal data of **FJI-H14** was collected on a SuperNova diffractometer at 100 K. The structure was solved using *SHELXT-2014* and refined by full-matrix least squares on  $F^2$  with *SHELXL-2014*<sup>57</sup>. All the non-hydrogen atoms were refined anisotropically. Hydrogen atoms of the organic ligands were generated theoretically on the specific atoms and refined isotropically. We employed *PLATON/SQUEEZE*<sup>58</sup> to calculate the contribution to the diffraction from the solvent region and thereby produced a set of solvent-free diffraction intensities. The final formula was calculated from the *SQUEEZE* results combined with elemental analysis data and TGA data. Crystallographic data and structure refinement parameters for this crystal are summarized in Supplementary Table 1.

**Gas-adsorption.** Low-pressure (<1 bar) adsorption measurements were performed using an Accelerated Surface Area and Porosimetry 2020-M System. Before the measurements, about 100 mg solvent-exchanged samples were loaded into the sample tube and then degassed under dynamic vacuum at 100 °C for 10 h to obtain fully desolvated samples. Low-pressure  $N_2$  adsorption isotherms were measured at 77 K in a liquid nitrogen bath (Supplementary Fig. 6). Low-pressure  $CO_2$  adsorption isotherms were measured at 195, 273, 283, 288, 291, 293, 298 and 308 K. The specific surface areas were determined using the BET model from the  $CO_2$  adsorption isotherm.

**The isosteric heat of adsorption.** Method 1: the isosteric heat of adsorption  $Q_{st}$  was calculated using the Clausius–Clapeyron equation (equation (1)).

$$\ln(P_i) = Q_{st} \times \frac{1}{RT_i} + C, \quad (1)$$

where  $P_i$  is the pressure of the isotherm  $i$  (kPa),  $T_i$  is the temperature of isotherm  $i$  (K),  $R$  is the gas constant and  $C$  is a constant. The  $Q_{st}$  is subsequently obtained from the slope of plots of  $\ln(P_i)$  as a function of  $1/T$  (Supplementary Fig. 7 and Supplementary Table 4).

Method 2: the  $Q_{st}$  was estimated from isotherms at different temperatures applying the Virial fitting method (equation (2) and Supplementary Fig. 8). The fitting parameters were then used to calculate the  $Q_{st}$  using equation (3).

$$\ln P = \ln N + \frac{1}{T} \sum_{i=0}^m a_i N^i + \sum_{i=0}^n b_i N^i, \quad (2)$$

$$Q_{st} = -R \sum_{i=0}^m a_i N^i, \quad (3)$$

where  $P$  is the pressure (mmHg),  $N$  is the adsorbed quantity ( $mg\ g^{-1}$ ),  $T$  is the temperature (K),  $R$  is the gas constant,  $a_i$  and  $b_i$  are virial coefficients and  $m$  and  $n$  represent the number of coefficients required to adequately describe the isotherms (herein,  $m = 5$ ,  $n = 2$ ).

**Calculation of gas selectivity based on IAST.** The gas adsorption isotherms were first fitted to a Langmuir–Freundlich model. IAST starts from the Raoult's Law type of relationship between fluid and adsorbed phase.

$$P_i = P y_i = P_i^0 x_i, \quad (4)$$

$$\sum_{i=1}^n x_i = \sum_{i=1}^n \frac{P_i}{P_i^0} = 1, \quad (5)$$

where  $P_i$  is the partial pressure of component  $i$  (kPa),  $P$  is the total pressure (kPa),  $y_i$  and  $x_i$  represent mole fractions of component  $i$  in gas and adsorbed phase (dimensionless).  $P_i^0$  is the equilibrium vapor pressure (kPa).

In IAST,  $P_i^0$  is defined by relating to spreading pressure  $\pi$ ,

$$\frac{\pi S}{RT} = \int_0^{P_i^0} \frac{q_i(P_i)}{P_i} dP_i = \Pi (\text{Constant}), \quad (6)$$

where  $\pi$  is the spreading pressure,  $S$  is the specific surface area of adsorbent ( $m^2\ g^{-1}$ ),  $R$  is the gas constant,  $T$  is the temperature (K) and  $q_i(P_i)$  is the single component equilibrium obtained from the isotherm ( $mg\ g^{-1}$ ).

The isotherm parameters are known from the previous fitting. The adsorption selectivities  $S_{ads}$  were calculated using equation (7).

$$S_{ads} = \frac{q_1/q_2}{P_1/P_2}. \quad (7)$$

In this study, IAST calculations were carried out assuming  $CO_2/N_2$  (15/85) binary mixed gases at 298 K and pressure up to 1 bar to mimic the composition and condition of flue gas for post-combustion  $CO_2$  capture.

**Computational methodologies.** The GCMC simulations for  $CO_2$  at 195, 273 and 298 K and up to 100 kPa were performed using with *RASPA* v2.03<sup>59</sup>. The **FJI-H14s** framework was generated in the  $R3$  space group based on the crystallographic data of **FJI-H14** to avoid disorder in the structure (Supplementary Fig. 14). Twelve unit cells of **FJI-H14s** ( $2 \times 2 \times 3$ ) were used to construct the simulation box of the GCMC run. The structural parameters of simulation box are  $a = b = 44.9714\ \text{\AA}$  and  $c = 33.1527\ \text{\AA}$ , as well as  $\alpha = \beta = 90^\circ$  and  $\gamma = 120^\circ$ . The partial charges on the framework atoms were calculated by the Gaussian09 software at the B3LYP/6-31 G\* level of theory<sup>60</sup>. Partial atomic charges were extracted using the ChelpG method by fitting them to reproduce the electrostatic potential generated by the DFT calculations. The charge was adjusted slightly in order to result in a neutral framework. Resulting partial charges for **FJI-H14s** are given in Supplementary Table 5.

$CO_2$ - $CO_2$  and  $CO_2$ -framework interactions were calculated using a Lennard–Jones (LJ) + Coulomb potential. LJ parameters for the framework atoms were taken from the Dreiding Force Field except for the copper atom, for which the parameters were taken from UFF (Supplementary Table 7). The  $CO_2$  LJ parameters were taken from an empirical TraPPE force field with a partial charge on each atom (Supplementary Table 6). The mixing LJ parameters between different atomic types were calculated according to the Lorentz–Berthelot mixing rule. Lorentz–Berthelot mixing rules were used for all cross terms, and LJ interactions beyond  $12.8\ \text{\AA}$  were neglected. The Ewald sum method was used to compute the electrostatic interactions. The fugacity of  $CO_2$  was calculated using the Peng–Robinson equation of state with the corresponding parameters. Simulations for  $CO_2$  adsorption used 100,000 cycles for equilibration and 100,000 cycles for data collection. In a cycle,  $N$  Monte Carlo moves were performed, where  $N$  is whichever value is larger between 20 and the number of molecules in the system. Monte Carlo moves used with equal probability were translation, rotation, insertion, deletion, and random reinjection of an existing molecule at a new position, while framework atoms remained fixed at their original positions.

The simulated isosteric heats of adsorption are computed from the GCMC simulations using the expression (equation (8)).

$$Q_{st} = RT - \frac{\langle U_{gg}N \rangle - \langle U_{gg} \rangle \langle N \rangle}{\langle N^2 \rangle - \langle N \rangle^2} - \frac{\langle U_{gf}N \rangle - \langle U_{gf} \rangle \langle N \rangle}{\langle N^2 \rangle - \langle N \rangle^2}, \quad (8)$$

where the brackets  $\langle \rangle$  denote the ensemble average,  $R$  is the gas constant,  $N$  is the number of gas molecules in the system,  $U_{gg}$  is gas–gas interaction energy and  $U_{gh}$  is the gas–framework interaction energy. The second and third terms are the contributions to the simulated  $Q_{st}$  from the gas–gas interaction and the gas–framework interaction, respectively.

DFT methods help shed light on adsorption mechanisms by calculating the adsorption energy of  $CO_2$  in MOF. Three possible main adsorption sites for adsorbed  $CO_2$  in MOF were investigated by the Dmol<sup>3</sup> module integrated into the Material Studio 7.0 program package<sup>61</sup>. The PBE-type exchange–correlation functional<sup>62</sup> with a generalized gradient approximation and the Double Numerical plus polarization (DNP) basis sets<sup>63</sup> that include a d-type polarization function on all non-hydrogen atoms and a p-type polarization function on all hydrogen atoms were employed for all calculations<sup>64</sup>. The FINE quality mesh size was employed in the calculations. During the  $CO_2$ -MOF structure optimization, the lattice parameters and the atomic fraction positions of the MOF crystal were kept immobile and the single  $CO_2$  molecule was allowed to move during optimization. The possible adsorption sites are shown in the Fig. 4d–f. The adsorption energies were calculated in terms of equation (9)

$$E_{ads} = E_{MOF-CO_2} - E_{MOF} - E_{CO_2}, \quad (9)$$

where  $E_{MOF-CO_2}$  stands for the energy of the optimized adsorbate-MOF structure, and  $E_{MOF}$  and  $E_{CO_2}$  denote the energies of the bare MOF structure and the isolated  $CO_2$  molecule, respectively. According to this equation, a more negative adsorption energy means more favorable binding.

**Catalyzation of cycloaddition of simulated post-combustion  $CO_2$ .** 20 mmol styrene oxide, 0.48 mol% per Cu(II) units (for example, 18 mg activated **FJI-H14** (0.016 mmol), 8.7 mg Cu(OAc)<sub>2</sub> (0.048 mmol)), and 164 mg TBAB (0.5 mmol, 2.5 mol%) were placed in a 5 mL dry Schleck tube with condenser, then 1 atm simulated post-combustion flue gas ( $CO_2 = 0.15\ \text{atm}$ ,  $N_2 = 0.85\ \text{atm}$ ) was introduced by bubbling, and the reaction mixture was stirred at 80 °C for 24 h.

**Uptake of different reactants.** 10 mg of activated crystals of **FJI-H14** was placed in a dry 5 ml Schleck flask, the flask was then evacuated under dynamic vacuum at 80 °C for 2 h and filled with argon, then 1 ml reactant was injected and the reaction was kept under argon atmosphere. 10 min later, the inclusion crystals of **FJI-H14** were filtered, after removing surface reactant molecules; the inclusion reactants can be readily removed from inclusion crystals **FJI-H14** by ultrasonic processing in DMSO- $d_6$  solution and further determined by <sup>1</sup>H NMR. Finally, about 2.78  $\mu\text{mol}$



of (chloromethyl)ethylene oxide, 1.2  $\mu\text{mol}$  of 1,2-epoxyoctane, or 1.1  $\mu\text{mol}$  of styrene oxide were added.

**Data availability.** The X-ray crystallographic coordinates for structure reported in this article have been deposited at the Cambridge Crystallographic Data Centre (CCDC), under deposition number CCDC 1517725. These data can be obtained free of charge from The Cambridge Crystallographic Data Centre via [www.ccdc.cam.ac.uk/data\\_request/cif](http://www.ccdc.cam.ac.uk/data_request/cif).

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## Author contributions

Q.C., D.Y. and M.H. conceived and designed the experiments and co-wrote the paper. L.L. performed most of the experiments and analyzed data. C.L. worked on all computational simulations. H.X., J.Q. and L.Z. performed adsorption test. Q.C., D.Y., J.F., H. J., M.H. and L.L. analyzed the data and wrote the manuscript. All authors discussed the results and commented on the manuscript.

## Additional information

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